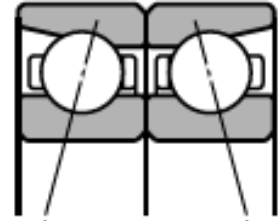


# Tutorial: Calculation of paired angular contact bearings

A pair of angular contact ball bearings mounted back-to-back should be calculated for a load case radial load only, and a second load case tilting moment only. The bearings have a build in pretension which is further increased by mounting and temperature.



## Bearing geometry

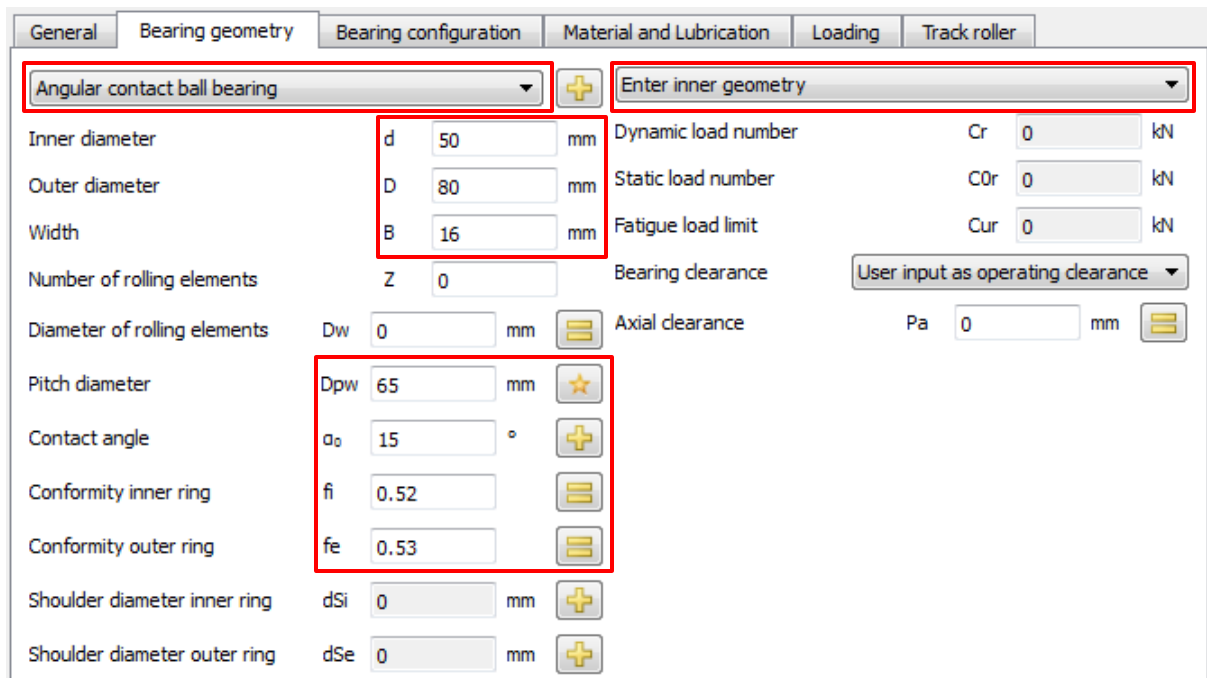
The bearing geometry for an angular contact bearing 7010C is provided as given in following table:

	Parameter	Value	Unit
Inner diameter	d	50	mm
Outer diameter	D	80	mm
Width	B	16	mm
Nominal contact angle	$\alpha$	15	°
Dynamic load capacity	Cr	28.2	kN
Static load capacity	C0r	20.2	kN
Fatigue limit	Cu	1.1	kN
Pretension	Fpre	4.2	kN
Tolerance		P4	
Tolerance shaft		k5	
Tolerance housing		H6	
Cage frequency at 60rpm	fc	0.435	Hz
Damage frequency inner ring at 60rpm	fip	10.733	Hz
Damage frequency outer ring at 60 rpm	fep	8.267	Hz
Damage frequency rolling element at 60 rpm	frp	7.319	Hz


This data is usually available for bearings and can be easily extracted from some manufacturers. To calculate the life of the bearing you should ask the manufacturer for additional data of inner geometry.

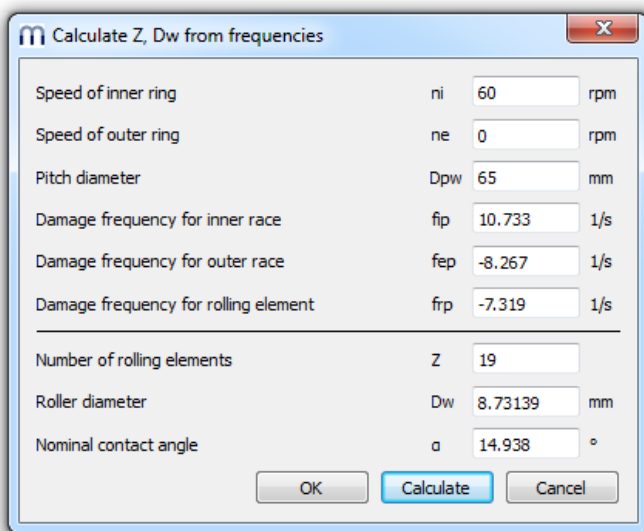
By selecting the tab corresponding to the page “Bearing geometry”, a first geometrical input will be set. Now click on the drop-down list on the left in order to choose the desired type of bearing, for this case “Axial angular contact ball bearing”. To proceed with the required input data, “Enter inner geometry” must be selected from the drop-down list on the upper right side of the page.

After introducing d, D und B, the user can automatically obtain the Pitch diameter, Dpw ( $Dpw = (50+80)/2 = 65\text{mm}$ ), when clicking the button.★ .



Since the conformity is not provided we use the values according to ISO/TS 16281 with  $f_i = 0.52$  and  $f_e = 0.53$

Now, the number of rolling elements  $Z = 19$  and the ball diameter  $D_w = 8.731$  will be figured out as the result of a backwards calculation by using the damage frequencies, which must be given to the software. To do so, a pop-up window is opened when pressing the button  located next to the "Dw" input, and then "Calculate" once the input data is filled out, and also OK to close the window.




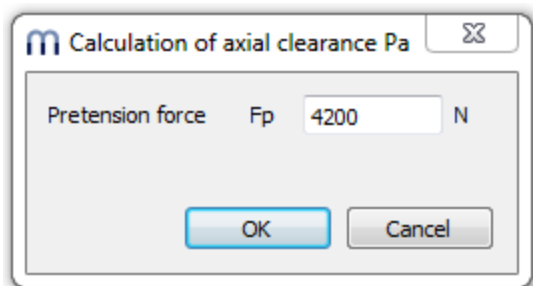
Note that  $D_w$  and  $\alpha$  must be manually rounded off on the page "Bearing geometry" so that they match standard values (The calculated  $D_w$  is practically equal to an usual one with  $11/32$  inch = 8.731mm, and the contact angle to  $15^\circ$ ).

After finishing the tutorial such a data can be checked at the report:

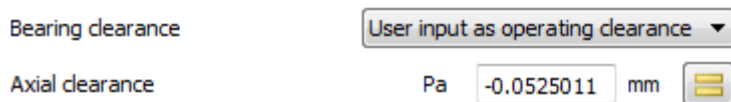
**Damage Frequencies**

Speed of inner ring	ni	1.000 1/s
Speed of outer ring	ne	0.0000 1/s
Rotation speed of cage	fc	0.4351 1/s
Damage frequency for inner race	fip	10.73 1/s
Damage frequency for outer race	fep	-8.2674 1/s
Damage frequency for rolling element	frp	-7.3194 1/s

A further unknown is the axial clearance of the bearing, since a pretension is given as a force. To calculate the axial clearance click on the conversion button  located by its side and calculate the axial clearance:



To get a pretension of 4.2kN we need an axial clearance  $P_a = -0.0525\text{mm}$ .



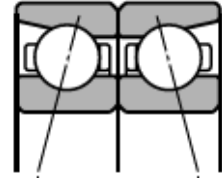
Now all the geometry of the bearing is given and both the tolerances and load capacities can be entered, so “Enter inner geometry and load capacity” and “User input” must be selected from the drop-down lists, as well as the desired Bearing tolerance. Both “Shoulder diameter inner ring” and “Shoulder diameter inner ring” will be shown after running the software.

General	Bearing geometry	Bearing configuration	Material and Lubrication	Loading	Track roller
Angular contact ball bearing		Enter inner geometry and load capacity			
Inner diameter	d	50	mm	Dynamic load number	Cr 28.2 kN
Outer diameter	D	80	mm	Static load number	C0r 20.2 kN
Width	B	16	mm	Fatigue load limit	Cur 1.1 kN
Number of rolling elements	Z	19		Bearing clearance	User input
Diameter of rolling elements	Dw	8.731	mm	Axial clearance	Pa -0.0525011 mm
Pitch diameter	Dpw	65	mm	Bearing tolerance	ISO 492 - P4
Contact angle	$\alpha_o$	15	°	Fit to shaft	k6
Conformity inner ring	fi	0.52		Surface roughness shaft	Rz 4 $\mu$ m
Conformity outer ring	fe	0.53		Shaft inner diameter	dsi 0 mm
Shoulder diameter inner ring	dSi	61.5076	mm	Fit to housing	H6
Shoulder diameter outer ring	dSe	68.4924	mm	Surface roughness housing	Rz 4 $\mu$ m
				Housing outer diameter	dhe 0 mm

The dynamic load capacity of the bearing given by the manufacturer is slightly larger than according ISO 281. Often manufacturers provide higher values than the standard to consider better material and quality. Therefore it is also possible to enter the values manually in addition to the calculation according to ISO 281.

## Bearing configuration

We have two bearings in back-to-back configuration. This can be defined on the page "Bearing configuration". Additional bearings can be added using the **+** button on the bottom right corner. The distance of the bearings from the origin is half of the bearing width, i.e.  $B/2=8\text{mm}$ . For a double row angular contact bearings also the bearing type "Angular contact bearing (double row)" could be used, but the bearing configuration also works for other configurations.



General Bearing geometry **Bearing configuration** Material and Lubrication Loading Track roller

Consider group of bearings

	Position [mm]	Axial Offset [mm]	Center of contact cone
1	-8	0	left
2	8	0	right

**+** **-** **✕**

An axial offset between the outer races can be defined additionally, if some additional pretension is introduced in the assembly. In this case we have no modification.

Running a calculation with zero load and opening the report, by pressing on the ⚡ and 📄 buttons, we will see the pressure between shaft and inner ring because of the interference fit and an increased pretension of the bearing of 5.79kN (also because of the interference fit. We already get a pressure of 2181MPa in the contact between balls and races:

Number	Fx [kN]	ux [mm]	Fy [kN]	uy [mm]	Fz [kN]	uz [mm]	My [Nm]	ry [mrad]	Mz [Nm]	rz [mrad]	pmax [MPa]	SF
1	5.79494	0.0000	0	0.0000	0	0.0000	0.00	0.00	0.00	0.00	2181.52	7.14
2	-5.79494	0.0000	0	0.0000	0	0.0000	0.00	0.00	0.00	0.00	2181.52	7.14

## Loading

We want to consider two load cases. The first one is a radial load of  $F_y = 15\text{kN}$ , the second a moment load of  $M_y = 300\text{Nm}$ . The speed of the inner ring should be  $n_i = 2200\text{rpm}$ . The temperature of the shaft should be  $50^\circ\text{C}$ , the temperature of the housing  $40^\circ\text{C}$ .

## Results for no loading

First we have a look at the results for zero loading. So press now on the tab "Loading" and enter just the aforementioned temperatures and inner ring speed.

General	Bearing geometry	Bearing configuration	Material and Lubrication	Loading	Track roller
Axial load	Fx	0 N	<input checked="" type="radio"/> Displacement	ux	0 mm <input type="radio"/>
Radial load	Fy	0 N	<input checked="" type="radio"/> Displacement	uy	0 mm <input type="radio"/>
Radial load	Fz	0 N	<input checked="" type="radio"/> Displacement	uz	0 mm <input type="radio"/>
Moment	My	0 Nm	<input type="radio"/> Rotation angle	ry	0 mrad <input checked="" type="radio"/>
Moment	Mz	0 Nm	<input type="radio"/> Rotation angle	rz	0 mrad <input checked="" type="radio"/>
Speed inner ring	ni	2200 rpm	<input checked="" type="checkbox"/> Inner ring rotates to load		
Speed outer ring	ne	0 rpm	<input type="checkbox"/> Outer ring rotates to load		
Temperature of shaft	Ti	50 °C	Temperature of housing	Te	40 °C

Result overview					
Basic reference rating life	L10r	26.3095	Basic reference rating life	L10rh	199.314 h
Modified reference rating life	Lnmr	88.5518	Modified reference rating life	Lnmrh	670.847 h
Maximal pressure	pmax	2343.89 MPa	Static safety factor	SF	5.75357

We already have a pressure of 2343MPa and a life of  $L_{10rh} = 199\text{h}$  only because of pretension.

## Radial loading

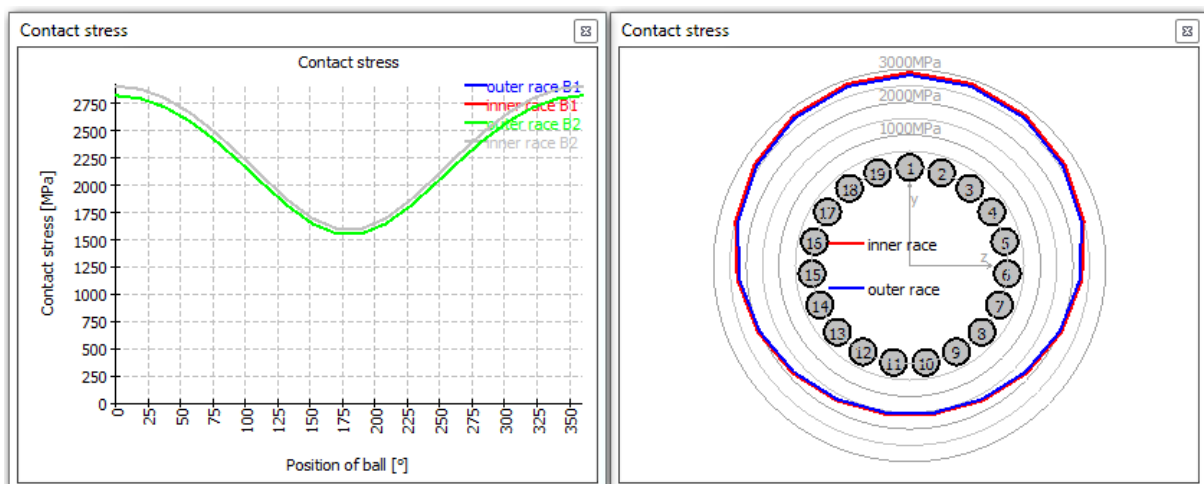
Entering the radial load of  $F_y = 15\text{kN}$  we get the following results:

General	Bearing geometry	Bearing configuration	Material and Lubrication	Loading	Track roller
Axial load	Fx	0 N	<input checked="" type="radio"/> Displacement	ux	0 mm
Radial load	Fy	15000 N	<input checked="" type="radio"/> Displacement	uy	0.0137175 mm
Radial load	Fz	0 N	<input checked="" type="radio"/> Displacement	uz	0 mm
Moment	My	0 Nm	<input type="radio"/> Rotation angle	ry	0 mrad
Moment	Mz	0 Nm	<input type="radio"/> Rotation angle	rz	0 mrad
Speed inner ring	ni	2200 rpm	<input checked="" type="checkbox"/> Inner ring rotates to load		
Speed outer ring	ne	0 rpm	<input type="checkbox"/> Outer ring rotates to load		
Temperature of shaft	Ti	50 °C	Temperature of housing	Te	40 °C

### Result overview

Basic reference rating life	L10r	11.5345	Basic reference rating life	L10rh	87.3827 h
Modified reference rating life	Lnmr	26.9023	Modified reference rating life	Lnmrh	203.805 h
Maximal pressure	pmax	2912.08 MPa	Static safety factor	SF	3.0001

The graphic contact stress shows that all balls are still loaded. To plot these charts, click on "Graphics" at the menu bar and select "Contact stress" and "Load distribution".



When performing the calculation according ISO 281 without pretension, we get a result of  $L_{10h} = 16666/2200 * (28.2 * 2^{0.7}/15)^3 = 215h$  instead of the  $L_{10h} = 87h$  with pretension by the software.

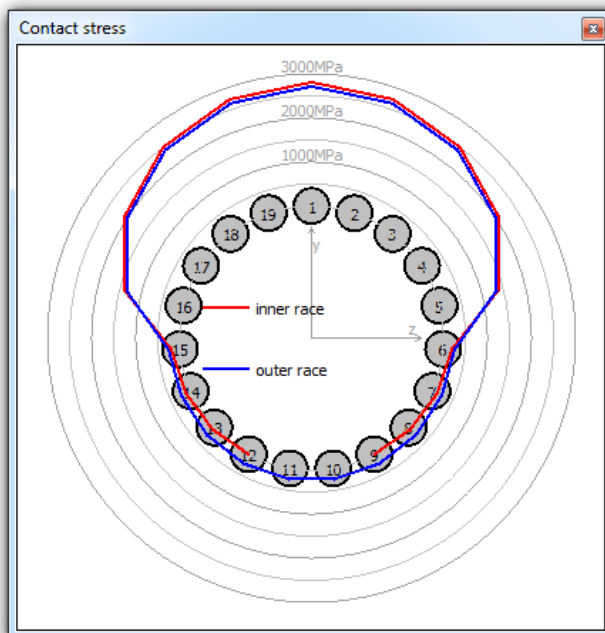
For the single bearings, we can see in the report that we have an axial (Fx), a radial (Fy) and a moment (Mz) load:

Number	Fx [kN]	ux [mm]	Fy [kN]	uy [mm]	Fz [kN]	uz [mm]	My [Nm]	ry [mrad]	Mz [Nm]	rz [mrad]	pmax [MPa]	SF
1	7.42436	-0.0009	7.5	0.0137	0	0.0000	0.00	0.00	-89.25	0.00	2912.08	3.00
2	-7.42436	0.0009	7.5	0.0137	0	0.0000	0.00	0.00	89.25	0.00	2912.08	3.00

Note that at “Bearing configuration” page, these kind of results can be also shown in additional cells by clicking the right mouse button and selecting them from the context menu:

General		Bearing geometry		Bearing configuration		Material and Lubrication		Loading		Track roller	
<input checked="" type="checkbox"/> Consider group of bearings											
	Position [mm]	Axial Offset [mm]	Center of contact cone		Fx [N]	pmax [MPa]					
1	-8	0	left		7424.36	2912.08					
2	8	0	right		-7424.36	2912.08					

If we do a calculation with operating clearance of zero for comparison (go to the “Bearing geometry” page and proceed as explained before, but now enter  $P_a = 0$  mm;  $F_p = 0$  N), we get a life of  $L_{10h} = 218h$ , which is close to the ISO 281 result. Now, as we can check in the graph of load distribution, the pretension is missing.





## Moment loading

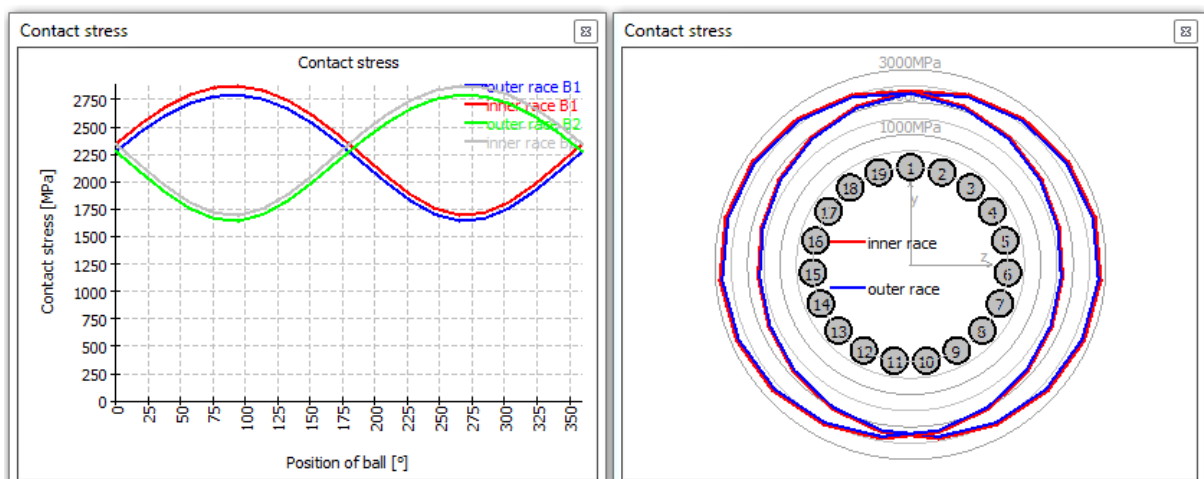
Now we run the same calculation with a moment loading of  $M_y = 300\text{Nm}$ .

General	Bearing geometry	Bearing configuration	Material and Lubrication	Loading	Track roller
Axial load	Fx	0 N	<input checked="" type="radio"/> Displacement	ux	0 mm
Radial load	Fy	0 N	<input checked="" type="radio"/> Displacement	uy	0 mm
Radial load	Fz	0 N	<input checked="" type="radio"/> Displacement	uz	0 mm
Moment	My	300 Nm	<input checked="" type="radio"/> Rotation angle	ry	0.610831 mrad
Moment	Mz	0 Nm	<input type="radio"/> Rotation angle	rz	0 mrad
Speed inner ring	ni	2200 rpm	<input checked="" type="checkbox"/> Inner ring rotates to load		
Speed outer ring	ne	0 rpm	<input type="checkbox"/> Outer ring rotates to load		
Temperature of shaft	Ti	50 °C	Temperature of housing	Te	40 °C

### Result overview

Basic reference rating life	L10r	12.5387	Basic reference rating life	L10rh	94.9903 h
Modified reference rating life	Lnmr	30.2859	Modified reference rating life	Lnmrh	229.439 h
Maximal pressure	pmax	2871.54 MPa	Static safety factor	SF	3.12897

The resulting life and pressure is similar to the calculation before, but now the load distribution is mirrored between the two bearings:



The single bearings have an axial load, a radial load and a moment load:

Number	Fx [kN]	ux [mm]	Fy [kN]	uy [mm]	Fz [kN]	uz [mm]	My [Nm]	ry [mrad]	Mz [Nm]	rz [mrad]	pmax [MPa]	SF
1	7.72831	-0.0009	0	0.0000	6.68603	0.0049	96.51	0.61	0.00	0.00	2871.54	3.13
2	-7.72831	0.0009	0	0.0000	-6.68603	-0.0049	96.51	0.61	0.00	0.00	2871.54	3.13

All the calculations were done using the medium operating clearance. On the first page "General" this could be changed into minimal or maximal clearance:


Reliability S  %  
 Calculation for medium clearance

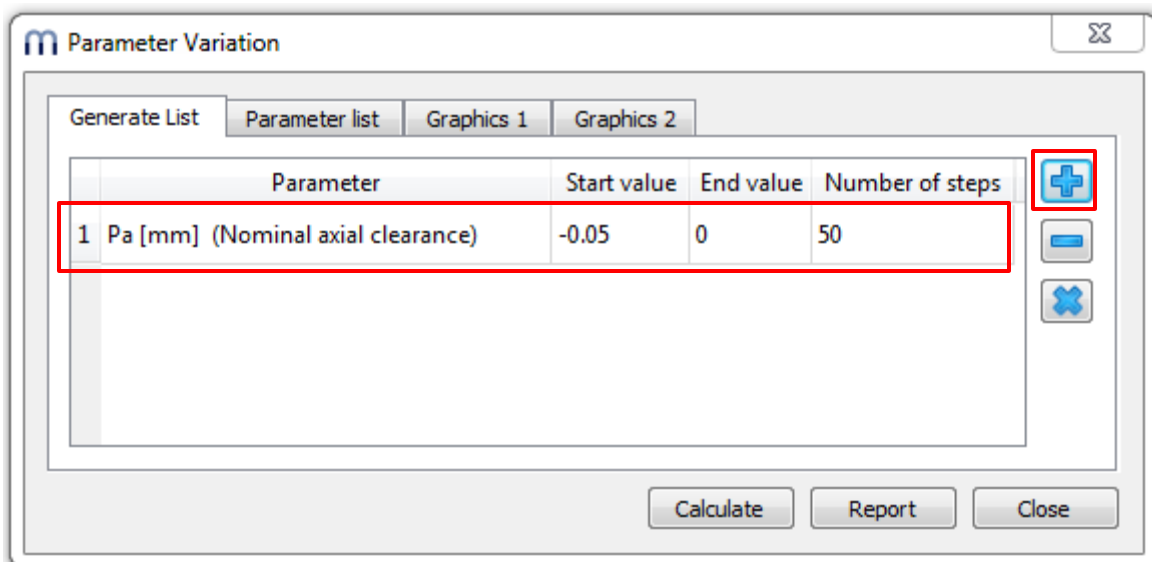
Considering the maximal clearance it could be decided if the pretension could be decreased, to increase the overall life.

## Further Analyses

### Optimization of life

The maximum bearing life can be found out by identifying and optimizing those parameters with a major influence in it. For this purpose, some features of the software can be easily used, thus enabling the user to reach an optimal configuration of the bearing.

For the case of moment loading ( $M_y=300\text{Nm}$ ), we will have a look on the nominal axial clearance, since the life has a great dependency on it. This way, we will use the parameter variation, so please select "Calculation" -> "Parameter variation". Now, in the tab page "Generate List", we add a parameter on the list, so we click on the -button and a new row is created. Doing a double-click on the first cell, a drop-down list is activated, then select "Pa[mm] (Nominal axial clearance)" from it. Please fill the row as shown:



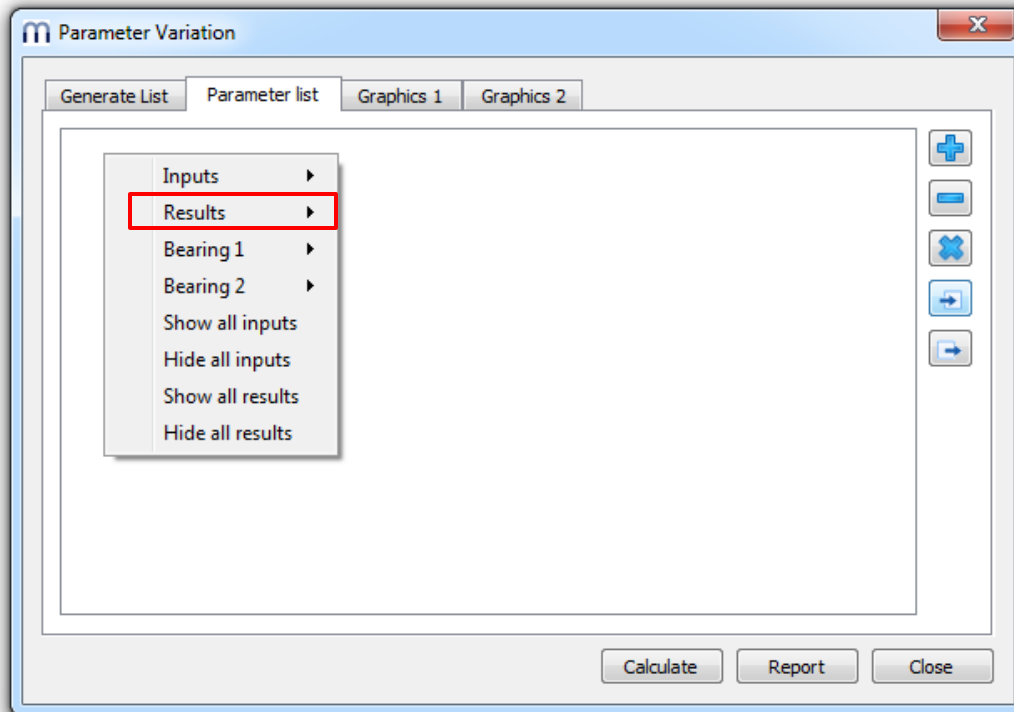
Parameter Variation

Generate List | Parameter list | Graphics 1 | Graphics 2

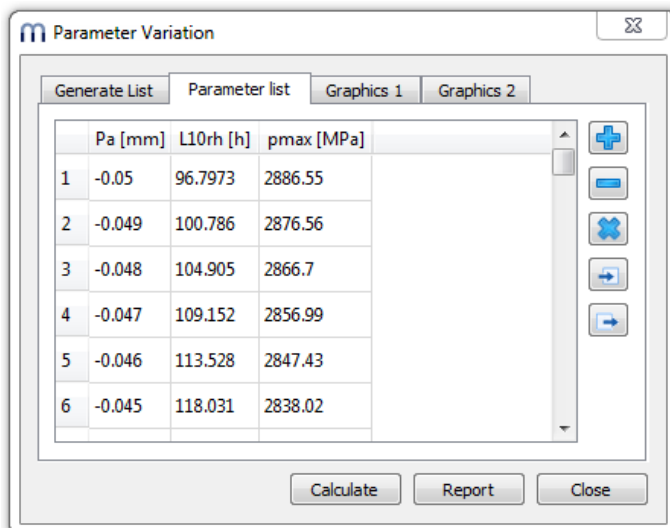
	Parameter	Start value	End value	Number of steps
1	Pa [mm] (Nominal axial clearance)	-0.05	0	50

Calculate Report Close

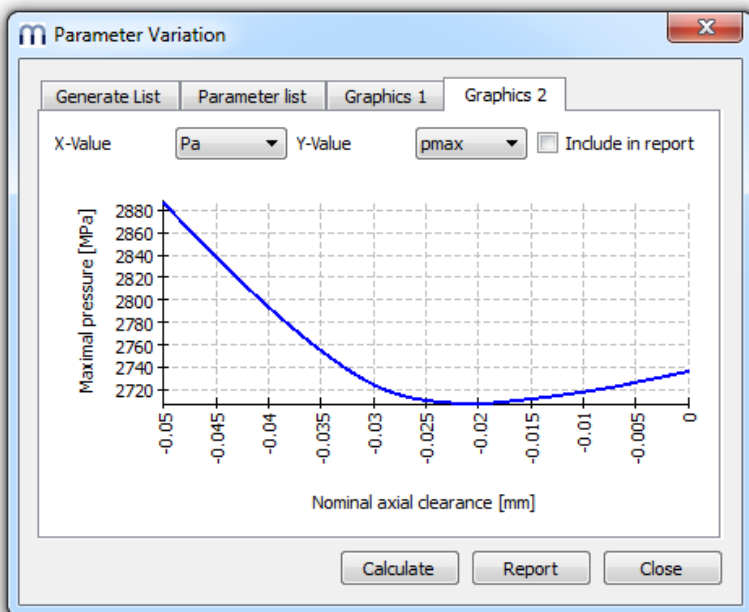
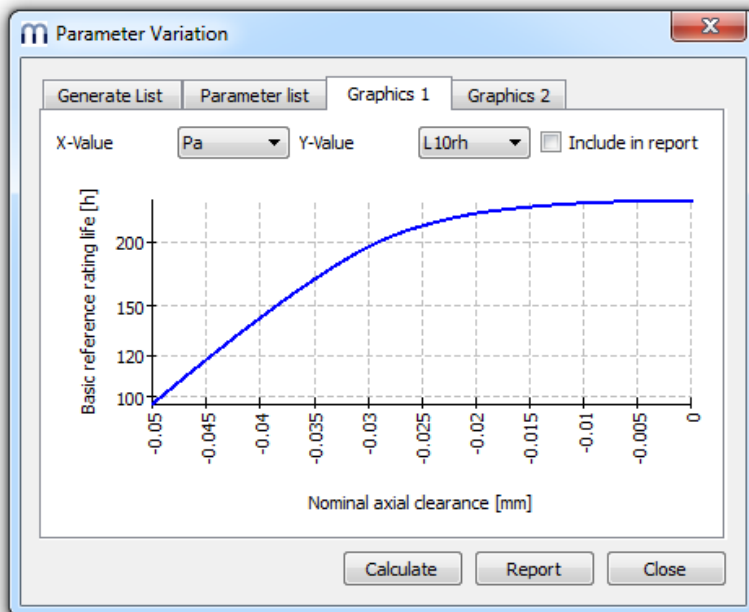
At the tab page “Parameter List”, do a right-button click and select “L10rh” and “Pmax” from the context menu “Results”.



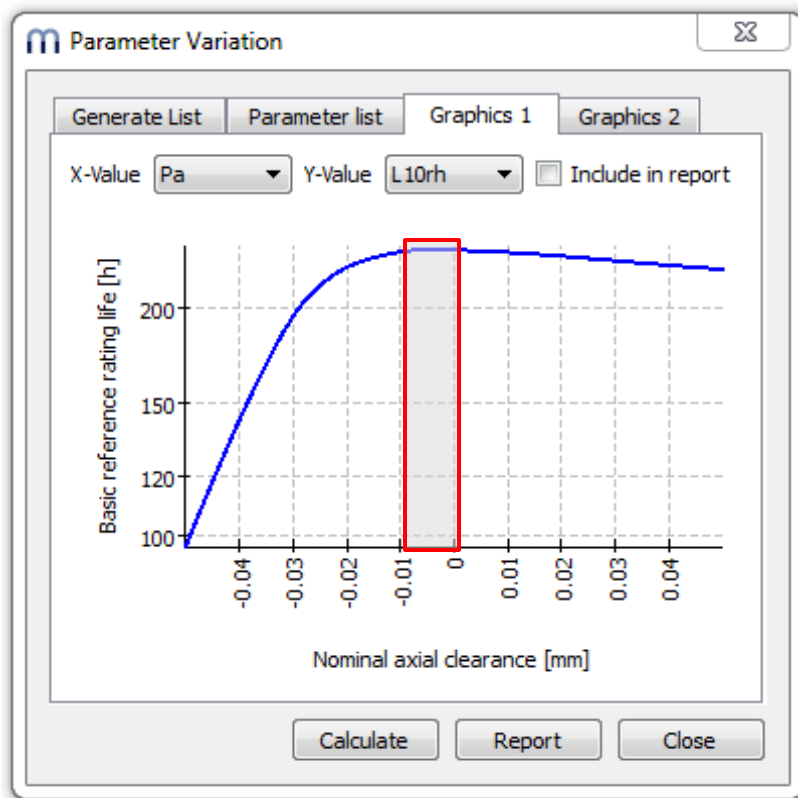
Now, Pressing “Calculate”, will generate a list of all parameter combinations and also run the analysis.



Selecting the tabs “Graphics 1” and “Graphics 2” we can visualize life over clearance or pressure over clearance.



For instance, in case we assume that the bearing must have a certain pretension, the user can deduce from this study, that the higher the pretension is, the shorter life the bearing has. However, if we widen the range of the possible axial clearances to the positive direction of X-Value for the bearing, we can identify a maximum over the range  $P_a = (-0.01, 0)$  mm:



## Load spectrum

A load spectrum can be used instead of a single load case. In order to activate this option in the software, go to the tab page “General” and activate the flag for “Use load spectrum”.

**mesys** **Rolling Bearing Calculation**  
Engineering Consulting Software AG  
Calculation of load distribution and reference life for rolling bearings considering ISO/TS 16281 and NREL/TP-500-42362

Project name:

Calculation description:

**Settings**

Limit for aISO: aISOMax  Reliability: S  %

Friction coefficient:  $\mu$   Calculation for medium clearance

Calculate lubricant film thickness  Oscillating bearing

Consider centrifugal force  **Use load spectrum**

Calculate required hardness depth  Calculate modified life

Use fatigue strength for hardness depth  Use extended method for pressure distribution

Required subsurface safety: Ssmin

Now go to the tab page “Loading”, click twice on the **+**-button in order to add two rows. By default, the column corresponding to “My [Nm]” is not activated, so do a right button click on the window and activate the flag for “enter My”; as a result of it, “ry[°]” will be hidden and “My [Nm]” will be shown in its stead. Now fill out the table as shown:

**mesys** **Rolling Bearing Calculation**  
Engineering Consulting Software AG  
Calculation of load distribution and reference life for rolling bearings considering ISO/TS 16281 and NREL/TP-500-42362

Project name:

Calculation description:

**Settings**

Limit for aISO: aISOMax  Reliability: S  %

Friction coefficient:  $\mu$   Calculation for medium clearance

Calculate lubricant film thickness  Oscillating bearing

Consider centrifugal force  Use load spectrum

Calculate required hardness depth  Calculate modified life

Use fatigue strength for hardness depth  Use extended method for pressure distribution

Required subsurface safety: Ssmin

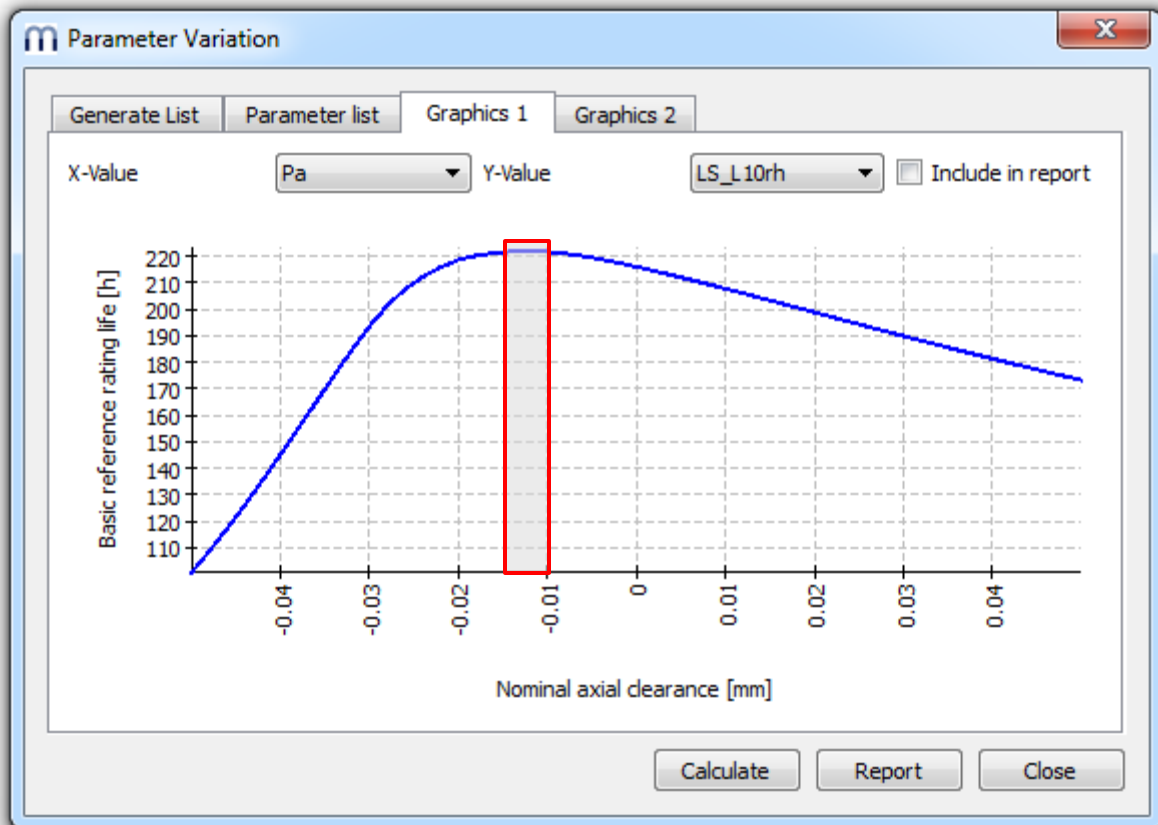
	Frequency	Fx [N]	Fy [N]	Fz [N]	My [Nm]	rz [°]	ni [rpm]	ne [rpm]	T <sub>i</sub> [°C]	T <sub>e</sub> [°C]	TOil [°C]
1	0.5	0	15000	0	0	0	2200	0	50	40	70
2	0.5	0	0	0	300	0	2200	0	50	40	70

enter Fx  
 enter Fy  
 enter Fz  
 **enter My**  
 enter Mz

inner Ring rotates to load  Outer ring rotates to load Results for No

We have set an equal distribution of load frequency for the current example, by entering "0.5" in each of the corresponding case cells.

Running the software calculation and carrying out a parameter variation study as we did before for the moment loading, it can be observed how the optimal axial clearance is now found over the range  $P_a = (-0.015, -0.01)$  mm:



Please note that for each load case, a full calculation using all factors is made. The resulting life is calculated using the life of each element.